FREQUENCY AT WHICH VAPOR BUBBLES

FORM DURING BOILING

V. F. Prisnyakov

An expression is found for the frequency at which vapor bubbles form; the familiar empirical dependences follow from this expression as particular cases. The theoretical results are in satisfactory agreement with experiment.

There is no general solution for the frequency f at which vapor bubbles form during boiling [1, 2]. Experimental studies are reported in [3-10], and the efforts which have been made to determine f are reviewed in [1, 2, 11, 12].

In determing f, many investigators have sought its connection with the rupture diameter D in the following form:

$$fD = C$$

where the quantity C has frequently been assumed a constant. According to [13], e.g., we have $C = 9.5 \cdot 10^{-2}$ m/sec; other values which have been reported are $7.87 \cdot 10^2$ m/sec for water and $7.62 \cdot 10^{-2}$ m/sec for CCl₄ [14], $8.38 \cdot 10^{-2}$ m/sec for methanol [15], 2.032 m/sec under natural-convection conditions during the boiling of a saturated liquid [16, 17], 0.1016 m/sec for methanol [18], and $8.8 \cdot 10^{-2} - 24.8 \cdot 10^{-2}$ m/sec during boiling of water at reduced pressure [10]. Contradictory dependences of C on the physical properties of the medium were reported in [12, 19-23].

It was shown in [24] that most of the published f and D results are not in satisfactory agreement with heat-transfer data because of incorrect averaging procedures: the arithmetic mean product $\langle fV \rangle$ increases with increasing heat flow q, and at certain q values we have fV = const for each bubble source.

Let us consider the growth of a bubble on the heating surface. During a time τ_d the bubble increases in size; after it reaches the rupture diameter D, it breaks off and enters the liquid. The volume it leaves is filled by a cooler liquid, which during a time τ_w is heated by an amount ΔT sufficient to begin the formation of a new bubble. The bubble formation frequency is

$$f = \frac{1}{\tau_{10} + \tau_{d}}$$

To determine the delay time $\tau_{\rm W}$ we assume that the liquid coming into contact with the heating surface is a semiinfinite mass. In this case the solution of the heat-transfer equation in the liquid layer yields the following relationship [25] between the heat flow q, the temperature drop ΔT , and $\tau_{\rm W}$:

$$\tau_{w}^{\circ} = \frac{\tau_{w}}{\tau_{*}} = \frac{\pi}{4} \left(\frac{J}{P} \right)^{2}$$

$$J = \frac{\Delta T c' \rho'}{r \rho''}, \quad P = \frac{g R_{*}}{r \rho'' a'}, \quad \tau_{*} = \frac{R_{*}^{2}}{a'}, \quad R_{*} = \left(\frac{\sigma}{g \left(\rho' - \rho'' \right)} \right)^{1/\sigma} \tag{1}$$

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To determine the bubble-growth time we use the equation

$$R = R_0 + \frac{4\varphi_0}{(2 + f_o)\sqrt{\pi}} J \sqrt{a'\tau} + \frac{2}{2 + f_o} \varphi_q \varphi_\rho \frac{q}{r \rho''} \tau$$
 (2)

Then we find (for $R \gg R_0$)

$$\begin{split} \tau_d &= \phi_1{}^2 \left(\frac{J}{P}\right)^2 \left[\left(1 + \phi_2 \frac{PR^\circ}{J^2}\right)^{1/2} - 1 \right]^2 \tau_*, \quad R^\circ = \frac{R}{R_*} \\ \phi_\theta &= \frac{1 + \cos\theta}{1 + ^{1/2} \cos\theta \left(2 + \sin^2\theta\right)} \;, \quad \phi_q = \frac{1}{2} \left(1 - \cos\theta\right), \quad f_\rho = 1 - \frac{\rho''}{\rho'} \\ \phi_1 &= \frac{2}{\sqrt{\pi} \left(1 - \cos\theta\right)} \;, \quad \phi_2 = \frac{\pi \left(1 - \cos\theta\right) \left(1 + ^{1/2}f_\rho\right)}{2\phi_\theta} \end{split}$$

For a large J > 10, Eq. (2) simplifies, and we can set

$$\tau_d = \frac{9\pi}{46} \frac{R^{\circ \circ}}{I^2} \tau_* \tag{3}$$

The rupture radius R° is given by

$$R^{\circ s} + \frac{3}{4} \frac{\zeta_w}{\zeta_g} N_{w'} \sin \alpha R^{\circ s} + \left(\frac{3}{8} \frac{\zeta_w}{\zeta_g} \varphi_w N_{w'}\right)^2 R^{\circ s} - \left(\frac{3}{2} \frac{\zeta_\sigma}{\zeta_g} \sin \theta\right)^2 R^{\circ s} - \frac{8}{9\pi^2} \times (1 + \cos \theta)^2 \sin \theta \frac{\zeta_R \zeta_\sigma}{\zeta_g^2} \vartheta J^4 R^\circ - \left[\frac{8(1 + \cos \theta)}{27\pi^2} \frac{\zeta_R}{\zeta_g} \vartheta\right]^2 J^s = 0$$

where

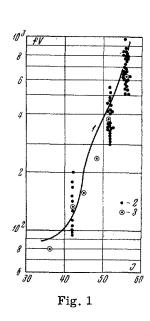
$$\begin{split} N_{w'} &= 9\varepsilon\Phi N_{w}, \ N_{w} = \frac{\rho'w^{2}}{V\operatorname{\sigma}g\left(\rho' - \rho''\right)} \\ \vartheta &= \frac{\rho'a'^{2}}{\sigma} \left(\frac{\sigma}{g\left(\rho' - \rho''\right)}\right)^{-1/2}, \ \varepsilon = \frac{15}{14} \left(1 + \cos\theta\right)^{1/2} \end{split}$$

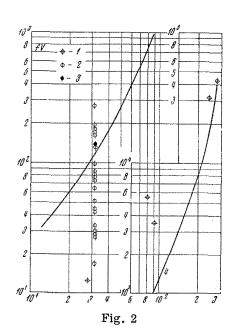
During boiling in a large volume on a horizontal surface, R° satisfies

$$R^{\circ \circ} - \frac{3}{2} \frac{\zeta_{\sigma} \sin \theta}{\zeta_{g}} R^{\circ} - \frac{8 (1 + \cos \theta)^{2} \zeta_{R} \theta J^{4}}{27 \pi^{2} \zeta_{g}} = 0$$
 (4)

Knowing R°, we can thus use Eqs. (1) and (3) to find the dimensionless rupture frequency $f^{\circ} = f\tau_{*}$; for large J, we have, approximately,

$$f^{\circ} = \left[\frac{\pi}{4} \left(\frac{J}{P}\right)^{2} + \frac{9\pi}{16} \left(\frac{R^{\circ}}{J}\right)^{2}\right]^{-1} \tag{5}$$





or, more accurately,

$$f_0 = \left(\frac{P}{J}\right)^2 \left\{\frac{\pi}{4} + \varphi_1^2 \left[\left(1 + \varphi_2 \frac{PR^\circ}{J^2}\right)^{1/2} - 1\right]^2\right\}^{-1}$$
 (6)

For J > 100, Eq. (4) yields $R^{\circ} \approx C_1 J^{4/3}$. In this case we can use Eq. (5) to find the equation analogous to the empirical dependence of [23], $fV \propto J^2$, for small q. If we have

$$^{3}/_{2}PR^{\circ}/J^{2}\gg 1\tag{7}$$

we can find from Eqs. (5) and (6) an expression analogous to the empirical dependence of [22]:

$$f^{\circ}R^{\circ 2} = 4\pi^{-1}J^{2}$$

If $R^{\circ} \propto J^{4/3}$, we find as a particular case, the equation [20, 21]

$$fR^{1/2} = \text{const}$$

If we have the inequality opposite (7), we find

$$f^{\circ} = \frac{4}{\pi} \left(\frac{P}{J} \right)^2$$

It follows that for small J, in which case R° is essentially independent of J, we have f = const, and at large J, for which we have R° $\propto J^{4/3}$, we find $fR^{3/2} = \text{const}$.

This brief analysis has shown that the exponent on R changes from 0 to 2; this result has been confirmed in particular cases [26].

An analysis [23, 24] has shown that we must seek the relationship between the frequency f and the volume of the detaching bubble, adopting as a parameter characterizing a particular vapor-formation center the product fV, the vapor-production rate of this center. To check these theoretical results, we therefore use plots of f° V $^{\circ}$ = f° R $^{\circ}$ vs J.

Figure 1 shows the experimental results of [24] (2), their average values (3), and a curve (1) calculated from the equations above. The agreement is seen to be satisfactory.

Figure 2 shows that the calculated results (3) and (4) agree with the experimental data of [10](1) and [27](2). (2).

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